

# Liquid-Solid Semi-Fluidization of Homogenous Mixtures — II: Prediction of Maximum Semi-Fluidization Velocity

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## ABSTRACT

The necessity of a generalized correlation for predicting the maximum semi-fluidization velocity is stressed. The experimental set up used for the study has been described in detail. Values of the maximum semi-fluidization velocity, obtained from the experimental data have been compared with those from theoretical equation, developed earlier for single sized particles and the deviations have been commented.

## INTRODUCTION :

The various aspects of liquid-solid semi-fluidization studied and reported earlier by different authors include the prediction of minimum and maximum semi-fluidization velocities, (1, 2, 3, 4) packed bed formation (5, 6, 7) and pressure drop across a semi-fluidized bed (8). Although considerable information is available for semi-fluidization characteristics of close-cut particles in liquid-solid system, literature related to the behaviour of mixed particles system is very limited (9).

Here an attempt has been made to calculate the maximum semi-fluidization velocities by the equation developed for single-sized particles incorporating suitable modifications and compare the same with the experimental values.

## Experimental set-up

The experimental set-up used in the present study is described in Fig. 1. The semi-fluidizer is a perspex column of 2.54 cms. inside diameter and 100 cms long inserted between two flanges and provided with an inclined feeder at a height of about 21 cms. from the base for intermediate addition and removal of materials to the column. A movable restraint made up of 100 mesh stainless steel screen is placed between two perspex rings, the outside diameter of which is very close to the inside diameter of the column. With the help of a 3 mm. diameter brass rod this restraint can slide to any position in the column. A rotameter is included in the liquid line and the fluid is recirculated by means of a pump. Two pressure taps, one just below the bottom

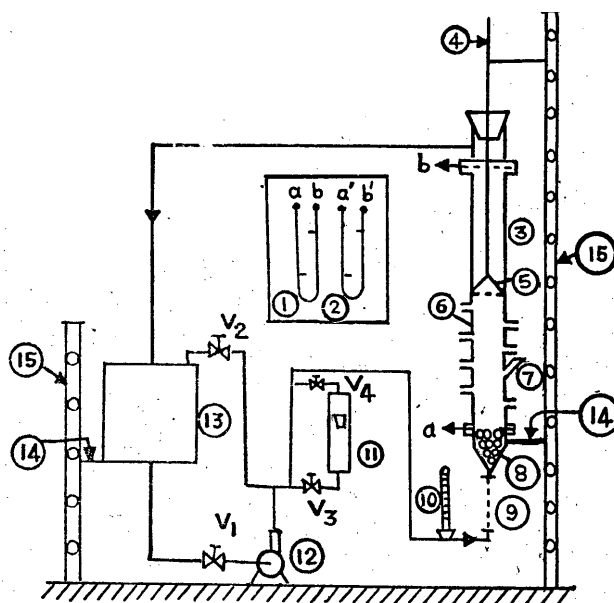


FIG. 1. SCHEMATIC DIAGRAM OF THE LIQUID-SOLID SEMI-FLUIDIZATION SET-UP

- 1 & 2. Manometers for bed pressure drop
  3. Semi-Fluidizer
  4. Movable Restraint Assembly
  5. Top Restraint
  6. Intermediate Pressure Tappings
  7. Inclined Feeder
  8. Distributor
  9. Flexible Connection
  10. Thermometer
  11. Rotameter
  12. Circulating Pump
  13. Liquid Reservoir
  14. Base Plate Support
  15. Supporting Structure
- a. b. Column Pressure Tappings  
 $V_1$ — $V_5$  Control Valves

screen and the other at the top of the column are provided to record the bed pressure drop. The inlet temperature of the liquid is noted by a thermometer.

## RESULTS AND DISCUSSION :

Altogether 32 sets of runs were taken using

TABLE — 1  
**CHARACTERISTICS OF MIXTURES AND RANGES OF VARIABLES STUDIED**

Material : Dolomite      Density : 2.83 gm/c.c.

Sl. No.	Mixture characteristics		Nomenclature	$(d_p)_{av}$ From eqn. (2)	R	cms. hs.
	Coarse (14/16 BSS)	Fine (44/52 BSS)				
1.	90	10	M <sub>1</sub>	0.1026		6.0
2.	70	30	M <sub>2</sub>	0.0870	2.0	6.0
3.	50	50	M <sub>3</sub>	0.0714	2.5	6.0, 8.0
			M <sub>4</sub>	0.0558	3.0	10.0, 12.0
4.	30	70			3.5	6.0
5.	10	90	M <sub>5</sub>	0.0402		6.0

various mixtures of a coarse (14/16 B.S.S.) and a fine (44/52 B.S.S.) size of dolomite particles to study the effects of various system parameters on  $G_{msf}$  (maximum semi-fluidization velocity) values. The mixtures can be called homogenous with respect to density as only one type of material was used. The characteristics of solid mixtures and ranges of variables studied are given in Table 1.

Based on exhaustive experimentation one of the authors has given the following correlation for the prediction of maximum semi-fluidization velocities for single sized particles in liquid solid system. (10).

$$G_{msf} = \frac{1.85 \times 10^4 (d_p)^{0.65} \rho_f (\rho_s - \rho_f)^{0.55}}{(\mu)^{0.1}} \quad (1)$$

The particle size ' $d_p$ ' in the above equation has been replaced by  $(d_p)_{av}$  and this has been calculated by using the equation (11).

$$(d_p)_{av} = \sum x d \quad (2)$$

With  $(d_p)_{av}$  the values of  $G_{msf}$  have been calculated by equation (1)

The experimental values of  $G_{msf}$  have been obtained from the packed bed formation Vs. mass velocity plots. It is observed that the maximum semi-fluidization velocity is little affected by both static bed height and the bed expansion ratio (Figs. 2 and 3 respectively). However, the mixture characteristics have profound influence on the maximum semi-fluidization velocity (Fig. 4).

The experimental values of  $G_{msf}$  have been compared in Table 2 with those obtained by equation (1) modified with respect to particle size by using  $(d_p)_{av}$  found from eqn. (2). The deviations lie within 7.5 to — 19.0. It is observed that in all the cases (except one) the experimental values are higher than the calculated ones. Maximum semi-fluidization velocities have been calculated on the basis of the average values of particle size whereas in an actual semi-fluidization experiment with mixtures, it is always possible that the fluid velocities necessary to lift the coarser particles will be higher than those calculated from the average particle diameters of the mixtures. The deviations are comparatively more for mixtures containing coarser components in the range of 30 — 70%.

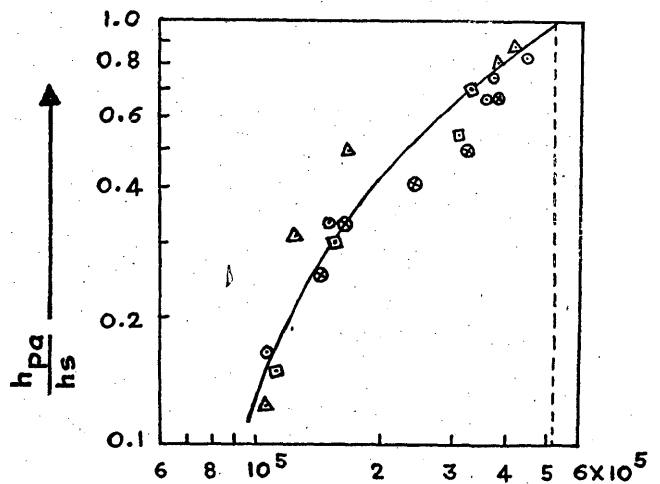


FIG. 2. EFFECT OF STATIC BED HEIGHT ON MAX SEMI-FLUIDIZATION VELOCITY

Fluid Mass Velocity,  $G$ , kg/Hr. M<sup>2</sup>.  
 System Dolomite-Water  
 Mixture Characteristics : M<sub>3</sub> (50 : 50)  
 Bed Expansion Ratio : R 2.5

LEGEND

- $h_{s1}$  ----- ○
- $h_{s2}$  ----- △
- $h_{s3}$  ----- □
- $h_{s4}$  ----- ⊗

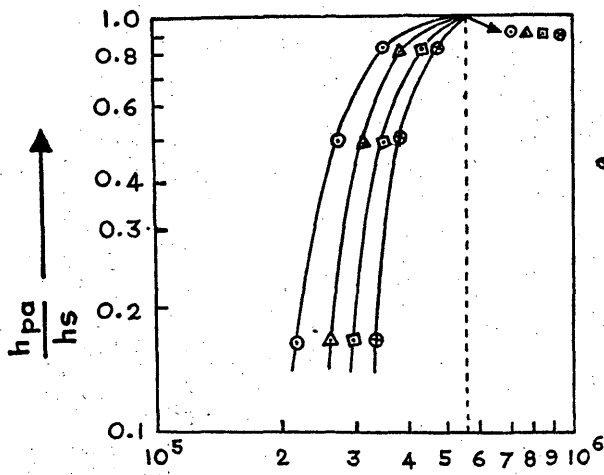


FIG. 3. EFFECT OF BED EXPANSION RATIO ON  $G_{max}$  SEMI-FLUIDIZATION VELOCITY

Fluid Mass Velocity,  $G$ , kg/Hr.  $M^2$ .  
System Dolomite-Water  
Static Bed Height : 6 cm.  
Mixture Characteristics  $M_1$  (10 : 90)

LEGEND

$R = 2$  -----  $\odot$   
 $R = 2.5$  ----  $\triangle$   
 $R = 3$  -----  $\square$   
 $R = 3.5$  ----  $\otimes$

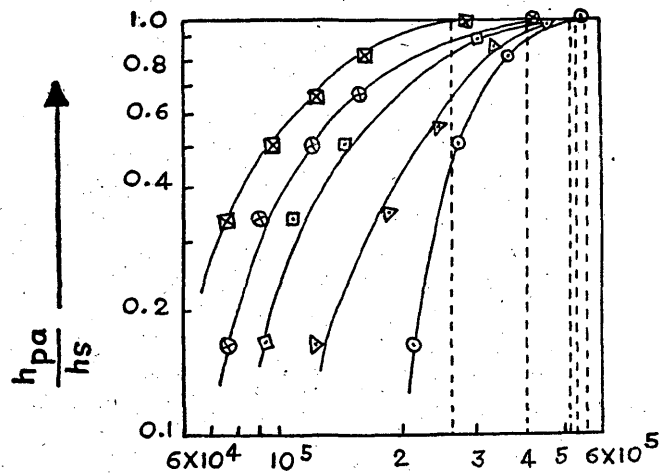


FIG. 4. EFFECT OF MIXTURE CHARACTERISTICS ON  $G_{max}$  SEMI-FLUIDIZATION VELOCITY

Fluid Mass Velocity,  $G$ , kg/Hr.  $M^2$ .  
System Dolomite-Water  
Static Bed Height :  $h_s = 6$   
Bed Expansion Ratio :  $R = 2$   
Mixture Characteristics .

LEGEND

$M_1$  -----  $\odot$   
 $M_2$  -----  $\triangle$   
 $M_3$  -----  $\square$   
 $M_4$  -----  $\otimes$   
 $M_5$  -----  $\boxtimes$

TABLE - 2  
COMPARISON OF THE MAXIMUM SEMI- FLUIDIZATION VELOCITIES

Sl. No.	Mixture characteristics	$G_{msf}$		Deviation of calculated values from the Experimental values
		From Expt.	Kg./hr ( $M^2$ ) From Eqn.	
1.	$M_1$	550000	524000	- 4.72
2.	$M_2$	520000	474000	- 8.84
3.	$M_3$	510000	414000	-18.82
4.	$M_4$	400000	354000	-11.50
5.	$M_5$	265000	285000	+ 7.55

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Nomenclature :

B.S.S. = British Standard Sieve  
 $D_c$  = Diameter of the semi-fluidizer, L  
 $d_i$  = Particle diameter, L  
 $(d_p)_{avg}$  = Average particle diameter for mixture, L

$G_{msf}$  = Maximum semi-fluidization velocity,  $ML^{-2}\theta^{-2}$   
 $h$  = Height of semi-fluidized bed, L  
 $h_s$  = Height of initial static bed, L  
 $M_1, M_2, \dots, M_5$  = Nomenclature for mixtures  
 $R$  = Bed expansion ratio in semi-fluidization dimensionless,  $h/h_s$   
 $x$  = Mass fraction of components of the mixture

**Greek Letters :**

$\rho_s$  = Density of solid,  $ML^{-3}$

$\rho_f$  = Density of fluid,  $ML^{-3}$

$\mu$  = Viscosity of fluid,  $ML^{-1}\Theta^{-1}$

$\Sigma$  = Summation

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