

Effect of Red Mud (RM) Reinforcement on Physio-Chemical Characteristics of Ordinary Portland Slag Cement (OPSC) Mortar

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Abstract:

The investigation focuses on evaluating the effect of varying % of red mud (RM) reinforcement with Ordinary Portland Slag cement (OPSC). Characterisation is done by adding 10, 20, 30, 40 and 50 % of RM by weight to OPSC. RM + OPSC composite mortars are made in an 8.5 × 5 × 4 cm³ cast iron mould with external vibration keeping water-binder ratio 0.4 by weight. The mortars are cured in water for 28 days and their physio-chemical characteristics are investigated. Mortar performances like compressive strength, hardness, XRD, FTIR, SEM are diagnosed. The composite mortars cementing properties are compared with original OPSC. The result reveals the augmentation of RM with OPSC increases the hydration capacity of OPSC with improved compressive strength. The experimental optimization shows a maximum value up to 10-20 % OPSC can be replaced by RM as filling material.

Key words:

Red mud, Cement, Compressive strength, XRD, FTIR, SEM.

1. Introduction

For last several years it is observed that ground granulated blast furnace slag has been widely used as a partial replacement for Ordinary Portland Cement (OPC) for concrete manufacturing. Slag as partial replacement in OPC in term uses the waste produced in steel industry, and hence reducing the carbon dioxide emissions produced during cement making [1]. In addition to that partial replacement of OPC by slag enhances certain physiological properties like, reducing heat of hydration and corrosion risk [2]. Many constituents are responsible for hydration of ordinary Portland cement paste. The calcium silicate hydrate (C-S-H) phase is the primary product of OPC hydration [3]. The amount of combined water (bound) present in OPC after hydration is dependent on phase composition of the original cement and on the degree of hydration [4]. Usually similar hydration products are found when OPC is partially replaced by slag [5]. But the amount of Ca(OH)₂ in OPC/slag composite are higher than in OPC pastes.

But it is worthy to discuss that ordinary Portland blast furnace slag cement (OPSC) is a mixture of ordinary Portland cement and not more than 65 weight % of granulated slag. It is generally seen that the hardening rate of slag cement is somewhat lower than OPC, for the first 28 days curing but then increases and after 12 months the compressive strength merges with OPC. As blast furnace slag is hydraulically weak, it has glassy structure and high alkaline medium is required to neutralize the silicate-aluminate network [6]. The idea of adding foreign materials like rice husk, silica fumes and zinc nanoparticles to OPSC is widely practised in order to reduce cost, conserve energy and protect environment. Literature reveals characterisation of Portland-blast furnace slag cement containing cement kiln dust and active silica [7]. An investigation on a variety of slag, fly ash and cement dust in the performance of industrial by products is reported [8]. Mechanisms and kinetic study of slag hydration in hydrated slag cement is available [9][10].

The outline for red mud reinforcement in OPC or OPSC is not revealed till. The red mud is generated as a by-product (waste) material in alumina production during bauxite purification by Bayer's process. A comprehensive outline of red mud applications is available [11]. The objective of this work is to evaluate the effect of partial substitution of OPSC by RM on its physio-chemical characteristic of the hardened composite pastes.

2. Experimental

2.1 Raw materials:

At incipient red mud was collected as wet powder form from NALCO, Damonjodi, India. The as received powder was dried under sunlight for 10 days to get moisture content up to 2 % by weight. The red mud powder was ball milled to a specific particle size below 50 μm diameter. The composition of red mud used can be collected from [12]. The OPSC was procured from Sarang market as Konark cement, manufactured by Odisha cement limited, Rajgangpur, India.

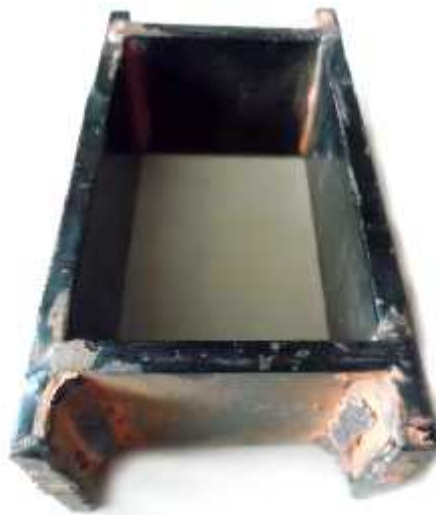


Figure-1 Snapshot of the matrix

2.2 Casting:

The red mud and cement mixture was prepared separately by varying the weight % of red mud as 10, 20, 30, 40 and 50. Each mixture was thoroughly blended using an in house V- shaped blender, in order to get a uniform composite powder. Thereafter each composite powder was stirred with distilled water using a mixture (Guangzhou Xuzhong Machinery Company limited). The water-binder ratio is maintained at a value of 0.4. The paste is poured into the cast iron mould to fill the entire volume. Casting was done by using a cast iron mould of size $8.5 \times 5 \times 4 \text{ cm}^3$. Captured image of the die used for casting is shown in **Figure 1**. Then the die was mechanically vibrated using external vibrator to achieve ultimate compaction of the paste. The die was removed immediately and composite bricks are allowed to harden for 2 days and then went for curing in normal water for 28 days at atmospheric condition.

3. Results and Discussion

3.1 Compressive strength and hardness:

Compressive strength is the most vital property to characterise the cement. The mortars were cut to cylindrical pieces having height to diameter ratio of 5.6. The specimen was compressed between the planets of the compression testing machine (Instron-1195) by application of load as per ASTM C39 standard. The results are shown in **Figure 2**, and compared with Indian standard IS 455-1989 designed for PSC. As normal PSC/OPSC bear a compressive strength of 33 MPa after 28 days of curing.

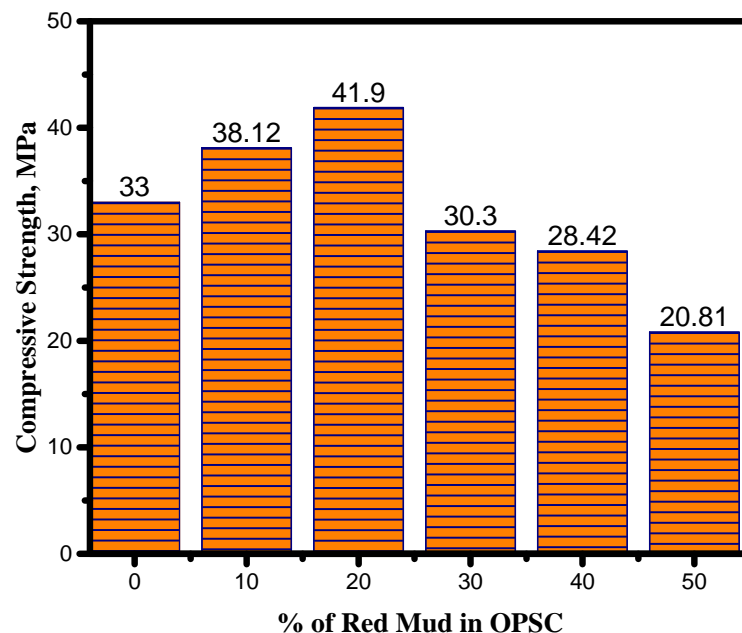


Figure-2. Variation of compressive strength with reinforcement of RM

The results reveal an improved compressive strength up to 20 % red mud reinforcement, might be due to improved hydration and structural properties approximating minimum air voids prevailing in the 20 % RM composite.

Hardness of the sample was determined using Vickers hardness test equipment (LHV-1000B), applying 50 gram load with 10 seconds indentation time. The results are reported in **Figure 3**. It is observed that hardness is extreme for 10 % red mud composite mortar. It is evident that the inclusion of RM to OPSC affects the rate at which it hydrates and changing its hardening properties.

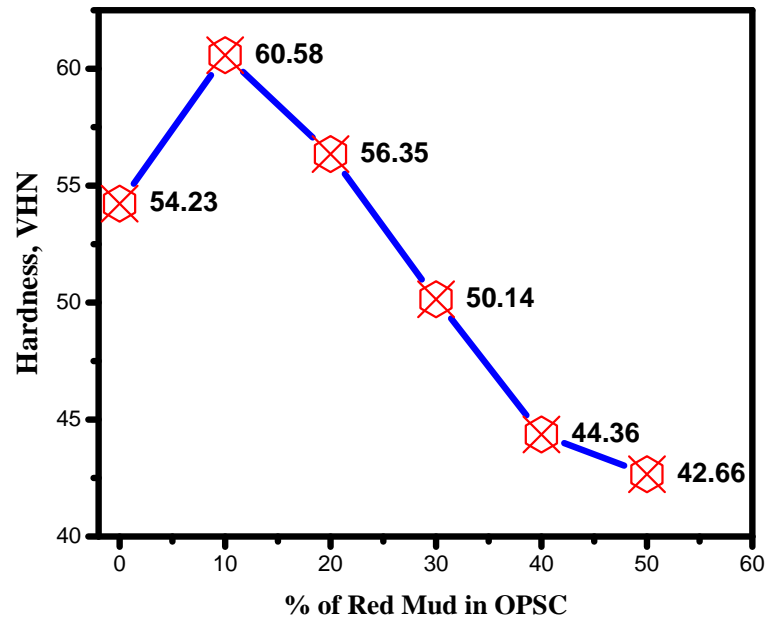


Figure-3 Hardness of OPSC and Composite mortars after 28 days curing.

3.2 XRD, FTIR, SEM

Figure 4(a) shows the XRD pattern of OPSC after 28 days hydration. The XRDs were captured using a Philips X-ray diffractometer. Emphasis is given to analyse only the phase compositions. It was seen that the primary phases OPSC builds up after 28 days hydration are Calcite (CaCO_3), Portlandite (Ca(OH)_2), Calcium Silicate Hydrate (C-S-H) and minor phases are Larnite (2CaO.SiO_2), Calcium Aluminate ($3\text{CaO.Al}_2\text{O}_3$) and Monosulphate hydrate ($3\text{CaO.Al}_2\text{O}_3.3\text{CaSO}_4.3\text{H}_2\text{O}$). Portlandite and Calcium silicate hydrate are formed after water hydration. But rest of the phases are also seen in OPSC powder [13]. **Figure 4(b)** and **Figure 4(c)** reveals the XRD patterns of 20 % RM + 80 % OPSC and 40 % RM + 60% OPSC composite mortars after 28 days hydration. Two new phases are found in the composite mortars as Hematite (Fe_2O_3) and Silicon dioxide (SiO_2), that red mud consistently poses. From the XRD analysis point of view; no new compound indicated, and there is no alternation in the phases by presence of RM particles was identified. Only revision of the relative intensities of the peaks was observed.

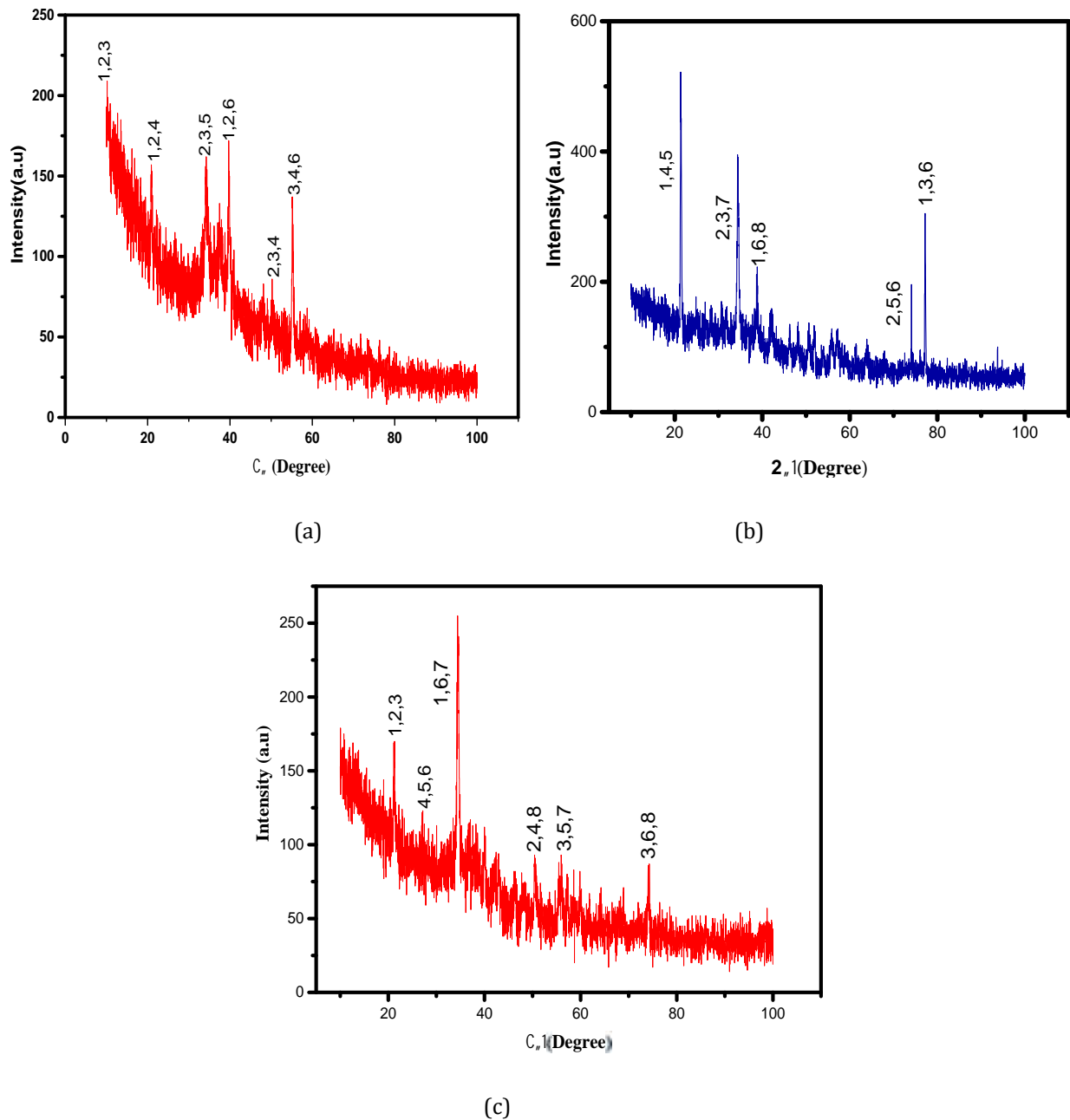


Figure-4. X-ray traces of (a) OPSC, (b) 20 % RM + 80 % OPSC, (c) 40 % RM + 60 % OPSC mortars. 1 Calcite CaCO_3 ; 2 Portlandite $\text{Ca}(\text{OH})_2$; 3 Calcium Silicate hydrate C-S-H; 4 Larnite $2\text{CaO} \cdot \text{SiO}_2$; 5 Calcium Aluminate $3\text{CaO} \cdot \text{Al}_2\text{O}_3$; 6 Monosulphate hydrate $3\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{CaSO}_4 \cdot 3\text{H}_2\text{O}$; 7 Hematite Fe_2O_3 ; 8 Silicon dioxide SiO_2 .

The IR characteristics of OPSC after 28 days hydration are identified and reported in **Figure 5.a** using FTIR analyser (thermo Scientific™ Nicolet™ iS™10) within the range of $500\text{-}4000\text{ cm}^{-1}$. **Table 1** reports the IR bands and their corresponding functional groups. **Figure 5.b** reveals the IR spectra of 20 % RM + 80 % OPSC composite mortar succeeded by 28 days hydration, their IR frequencies and assigned groups are dispersed in **Table 2**. Additional H-OH stretch (bound water) was observed for 20 % RM composite cement at 2923.76 and 1711.42 cm^{-1} band. This might be due to higher rate of

hydration with RM reinforcement. As the process of hydration is the progressive conversion of free (liquid) water in capillary pores in to bound water during the cement hydration. So it is a good approximation that inclusion of RM (up to 20 %) to OPSC minimizes the free water and increases bulk liquid water and structural (chemically bound) water. The C-S-H gel phase is responsible to carry significant amount of free and adsorbed water in its gel pores, and holds more tightly bound water within its inter particle spaces catalysed by RM.

Table 1 FTIR spectra of OPSC after 28 days hydration

Wave band, cm^{-1}	Assigned group
3406.92	(-O-H) stretch, H bonded
1448.56	Carbonate CO-stretch
964.49	Silicate SiO stretch
860.55	Carbonate CO bend
537.41	C-Br stretch

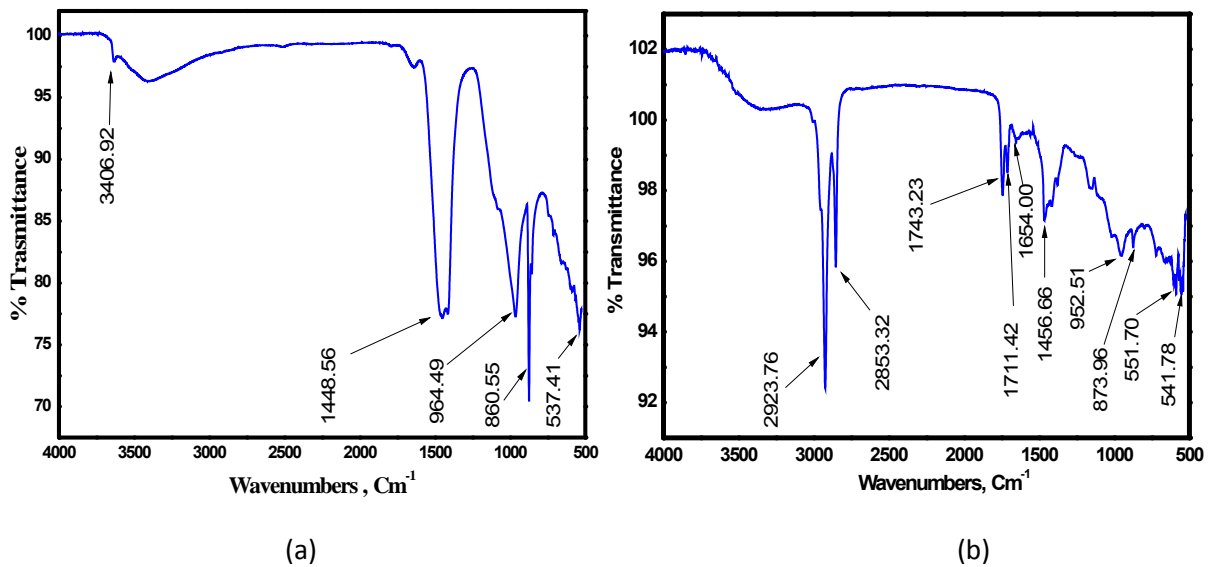


Figure-5 FTIR spectra of (a) OPSC and (b) 20 % RM + 80 % OPSC mortar

Table 2 IR spectra of 20 % RM + 80 % OPSC after 28 days hydration

Wave band, cm^{-1}	Assigned group
2923.76	Bound water (H-OH stretch)
2853.32	Bound water (H-OH stretch)
1743.23	CO_2 CO stretch
1711.42	Bound water HOH bend
1654.00	Bound water HOH bend
1456.66	Carbonate CO stretch
952.51	Silicate SiO stretch
873.96	Sulphate SO stretch
551.70	C-Br stretch
541.78	C-Br stretch

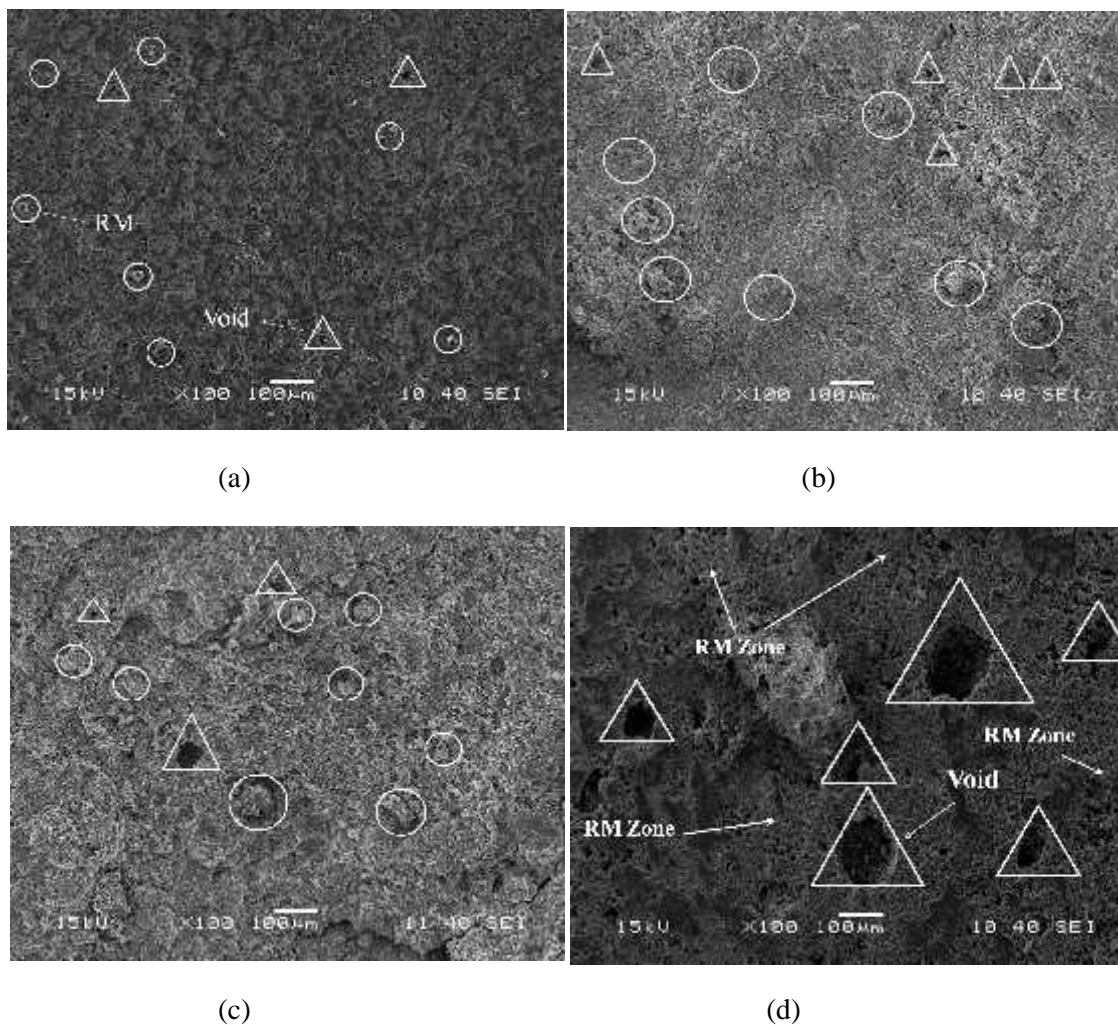


Figure-6 Microstructure of (a) 10 % RM + 90 % OPSC (b) 20 % RM + 80 % OPSC (c) 40 % RM + 60 % OPSC (d) 50 % RM + 50 % OPSC at $\times 100$ magnification

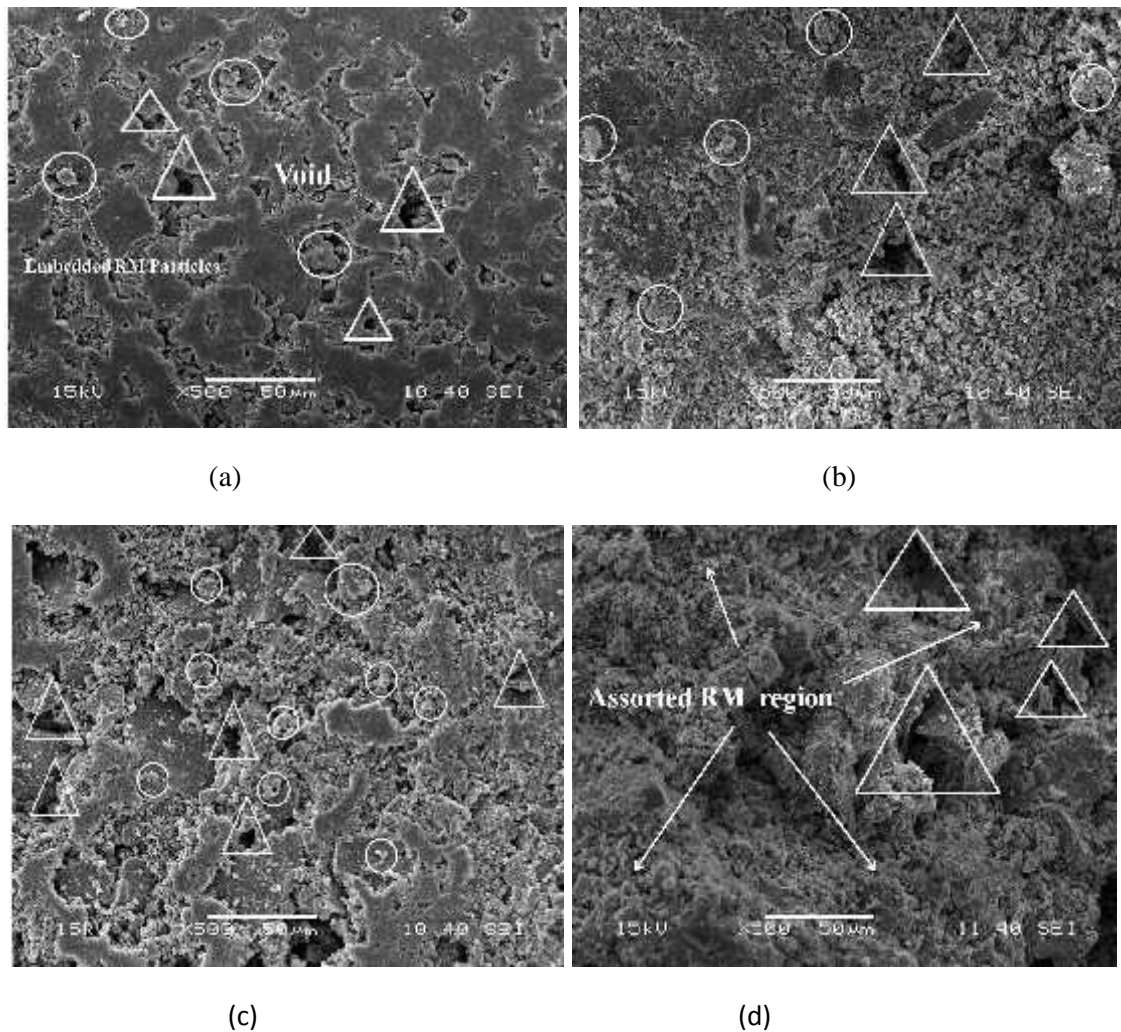


Figure-7 Microstructure of (a) 10 % RM + 90 % OPSC (b) 20 % RM + 80 % OPSC (c) 40 % RM + 60 % OPSC (d) 50 % RM + 50 % OPSC at $\times 500$ magnification

Morphology of composite mortars after 28 days hydration is captured using a SEM (Scanning Electron Microscope, JEOL; JSM-6480 LV). Microstructures are shown in **Figure 6-7**. For 10 % RM + 90 % OPSC composite; distribution of RM particles is relatively low. Quite low numbers, small size air voids (pores) are visible. Minimum amount of air voids are observed for 10-20 % RM reinforcement. Entrapped air voids (porosity) are seen to be increasing for further addition of RM. The entrapped air bubbles are formed in during mixing of water-binder and play a dominant role for their effect on the strength of the concrete. More isolated and bigger globular voids (large capillary pores) are seen for 50 % RM + 50 % OPSC mortar and hence lowering the effectiveness. The inclusion of RM (< 20 %) might be helping for increasing the C-S-H gel formation (including its internal gel pores) and thereby increasing the strength.

4. Conclusion

The combined use of XRD, FTIR and Scanning electron microscopy techniques reveal the output results for reinforcing red mud in OPSC. It permits to study the hydration of OPSC with red mud, evaluating the

variation of hydration rate and formation of phases if any. It is concluded that red mud inclusion in OPSC improves the hydration rate and increases the concrete strength. No chemical changes involved during hydration of the composite mortars, as no new phases are identified. The IR technique innovates more bound water existence during hydration with red mud, attributing to H-OH stretching. Thus red mud may be used for partial replacement of OPSC up to 20 % by weight and can be implemented as filling material, substituting OPSC.

Conflict of interest:

All authors declared that no conflict of interest exist for publishing this research paper.

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