

PROPERTY OPTIMIZATION OF FERROMAGNETIC SHAPE MEMORY ALLOYS WITH RESPECT TO COST

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ABSTRACT

Ferromagnetic shape memory alloys (FSMAs) are the interesting materials exhibiting shape memory effect and magnetism simultaneously. They show magnetic field-induced strains at room temperature greater than any magnetostrictive, piezoelectric or electrostrictive material, and faster frequency response than temperature driven shape memory alloys. Among various FSMA materials, Ni-Mn-X (X =Ga, In, Sn, Sb) have gained considerable interest due to their multifunctional properties such as shape memory effect, magnetocaloric effect, magnetoresistance, etc., associated with first order martensite to austenite structural transition. FSMA spread its application in broad area from aerospace industry to medical application, but not vividly use; because of its high cost. Ni-Mn-Sn FSMAs shows low cost of manufacturing due to its low value of constituting element. This paper investigates the behavior of Ni-Mn-Sn Heusler FSMA by varying the weight percentage of Sn. Three alloys i.e. $Mn_{50}Ni_{50-x}Sn_x$ ($x = 5, 7.5, \text{ and } 10$) were produced as bulk polycrystalline ingots by arc melting. In order to identify structural phases X-ray diffraction (XRD) measurements were conducted at room temperature using Cu K α radiation. By Differential Scanning Calorimetric (DSC) study it is found that, the transformation temperatures gradually decreases as increasing the Sn content, which shows it can apply in higher working temperature range than that of Ga-FSMAs.

Key words: Ferromagnetic Shape Memory Alloys (FSMAs), Ni-Mn-Sn, martensitic transformation.

1. INTRODUCTION

Ferromagnetic shape memory alloys (FSMAs) are the demanding material for magnetic actuator since one can obtain large reversible strains either through martensitic transformation or rearrangement of martensite variants induced by an external magnetic field. A Ni-Mn-Sn Heusler alloy has been found to undergo martensitic transformation at low temperature and the martensite phase has been found to have thermoelastic nature [1]. Thermoelastic martensite phase of Ni-Mn-Sn Heusler alloy has been recently shown to be capable of magnetic shape memory effect [2- 3]. The magnetic field-induced strain observed in these magnetic shape memory alloys differs

from conventional magnetostriction involving distortion of the crystal lattice. Magnetic shape memory effect in these materials involves the movement of twin boundaries which results in the growth of one of the twin variants at the expense of the other in response to an applied magnetic field below the martensitic transformation temperature. The crystal structure of Ni-Mn-Ga at high temperature phase (austenite) is L_2 with a cubic lattice, as shown in Figure-1. This stoichiometric phase undergoes a martensitic transformation at around 276 K. This diffusionless transformation results in a martensite phase with a tetragonal structure and the transformation is reversible [2]. A martensitic phase generally accommodates the strain associated with the transformation

by slip or by a formation of twin variants that pack together in compatible orientations to minimize strain energy between the martensitic region and the surrounding untransformed, highly symmetric parent phase.

In recent study Mn- based Heusler alloys have been focus as one of the typical magnetocaloric effect material. Among them, it is found that Ni-Mn-Sn SMA is a less cost material due to lesser cost of Sn element. By considering cost, the goal of this investigation is to find a magnetic alloy exhibiting a martensitic phase transformation that would provide a large controllable displacement with the application of low magnetic field at reasonable operating temperature. In many experiment Ni-Mn-Ga alloys are widely examined for which it serves as a reference alloy. But the Husler alloys the choice of Ni-Mn-Sn alloy is due to: (a) Ni-Mn-Sn not expensive as gallium, (b) It does not contain toxic as that of gallium [4], (c) Ni-Mn-Sn is less brittle than Ni-Mn-Ga [5], (d) Low transformation and curie temperature of stoichiometric Ni-Mn-Ga than Ni-Mn-Sn, (e) The austenite and martensite phase of Ni-Mn-Sn have the same crystal structure as the corresponding phases of Ni-Mn-Ga and have the same magnetically easy axis[6], (f) Ni-Mn-Sn alloys are known to have comparably high L_{21} / tetragonal transition temperature as that of Ni-Mn-Ga, (g) Stoichiometric of Ni-Mn-Sn alloys reveals similar magnetostrictive behavior with respect to temperature as that of Ni-Mn-Ga alloys[6], (h) Ni-Mn-Ga alloys is insufficient for FSMA actuators[7].

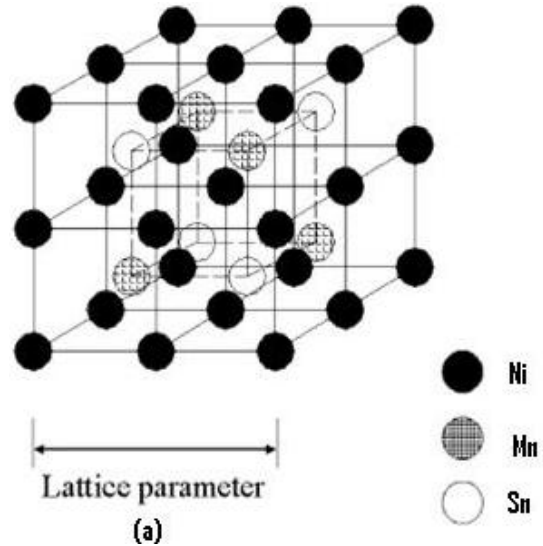


Fig 1. Unit cell of Ni-Mn-Sn (L2 phase) FSMA Heusler alloy at room temperature.

2. EXPERIMENTAL PROCEDURE

Three ternary intermetallic polycrystalline compound of composition $Ni_{50}Mn_{50-x}Sn_x$ ($x = 5, 7.5$ and 10) FSMA Heusler alloy was prepared by non-consumable arc-melting. The commercial purity of used Ni, Mn, Sn are 99.95%, 99.9% and 99.99% respectively. The melting was carried out under high purity atmosphere (99.996%). For the preparation of alloy ingot, the melting chamber was evacuated to a pressure about 10^{-5} torr and then was purged with pure argon. The process of evacuation and purging was repeated up to three times. The melting was carried out in an argon atmosphere and at a chamber pressure of nearly 500Mtorr. For complete homogenization of the alloy, the entire melting process was repeated several times. Then the alloy was cast into a rod form shown in Figure 2. The ingot was sealed in a quartz ampoule filled with helium gas and solutionized at $1000^{\circ}C$ for 24 hour for homogenization. The Martensitic Transformation and phase in these alloys successfully characterized by using X-Ray Diffraction and Differential Scanning

Calorimetry (DSC). DSC carried out in Mettler device working with a liquid nitrogen cooling system. In XRD, Cu-Ka radiation ($k=1.5418\text{\AA}$) used and was carried out in the interval $30^\circ \leq 2\theta \leq 75^\circ$ with a step increment of 0.05° .



Fig 2. Prepared Ni-Mn-Sn Heusler FSMA in Rod shape.

3. RESULTS AND DISCUSSION

3.1 Thermal analysis:

The transformation temperatures the alloy series $\text{Ni}_{50}\text{Mn}_{50-x}\text{Sn}_x$ ($x = 5, 7.5$ and 10) have been determined from DSC. In forward martensitic transformation, Martensitic start temperature (M_s) and Martensite finish temperature (M_f) are measured. Simultaneously in reverse martensitic transformation Austenite start temperature (A_s) and Austenite finish temperature (A_f) are measured. M_s , M_f , A_s and A_f temperature of prepared alloy are given in Table-1. The transition temperatures of these alloys are plotted in the diagrams of figure-3. It is observed that M_s , M_f , A_s and A_f decreases almost linearly by increasing the weight percent of Sn in the prepared alloy.

Table-1. Transformation temperature of Ni-Mn-Sn alloys.

Temperature($^\circ\text{K}$)	Sn_5	$\text{Sn}_{7.5}$	Sn_{10}
M_s	625	436	228
M_f	597	407	202
A_s	618	389	205
A_f	667	444	246

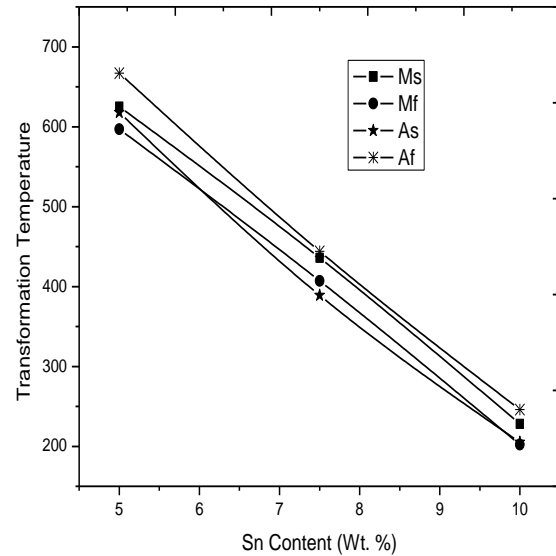


Fig 3. Thermal analysis of $\text{Ni}_{50}\text{Mn}_{50-x}\text{Sn}_x$ ($x = 5, 7.5$ and 10) series Alloy.

3.2 X-Ray study:

To determine the thermal analysis conditions it is important the knowledge of crystal structure at room temperature. So, XRD patterns were collected at room temperature by taking Cu-Ka radiation ($k=1.5418\text{\AA}$). XRD pattern of Sn_5 , $\text{Sn}_{7.5}$, Sn_{10} are given in Figure-4, 5 & 6. Miller indexes were assigned by using Philips-X'pert-Highscore and JCPDF Software. For Sn_5 alloy, the crystalline structure is Orthorhombic having lattice parameter $a=0.7888\text{nm}$, $b=0.5383\text{nm}$ and $c=0.5143$. For $\text{Sn}_{7.5}$ alloy, the crystalline structure is Orthorhombic and having lattice parameter $a=0.7862\text{nm}$, $b=0.5379\text{nm}$ & $c=0.5117\text{nm}$. For Sn_{10} alloy, the crystalline structure is L_{21} , which shows austenitic phase and its lattice parameter, $a=0.5997\text{nm}$. In Sn_5 & $\text{Sn}_{7.5}$ alloys the phase is found orthorhombic, but their relative peaks intensity is different. It is known that Heusler alloys sometimes present texture effects [8]. In Sn_{10} alloy, the peaks reflections indexed as $3\ 1\ 1$ and $3\ 3\ 1$ confirms the existence of the highly ordered L_{21} structure. From XRD diffraction

patterns it is clear that DSC scans of alloys Sn5 and Sn7.5 should be performed by heating from room temperature in order to detect the martensite-austenite transition. Similarly, DSC scan of alloy Sn10 should be performed by cooling from room temperature.

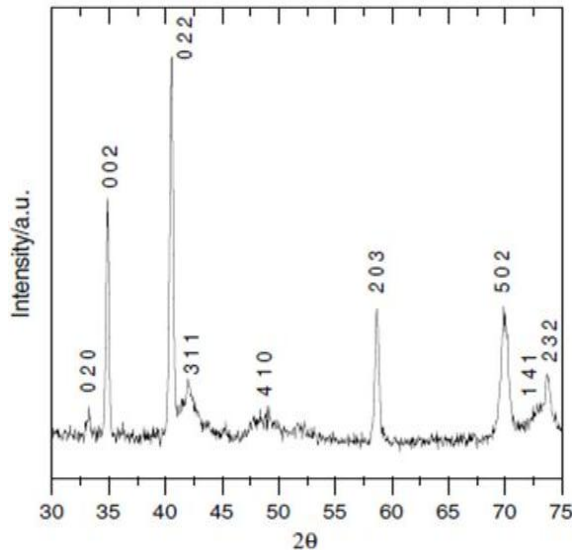


Fig 4. X-ray diffraction pattern of $Mn_{50}Ni_{45}Sn_5$ alloy.

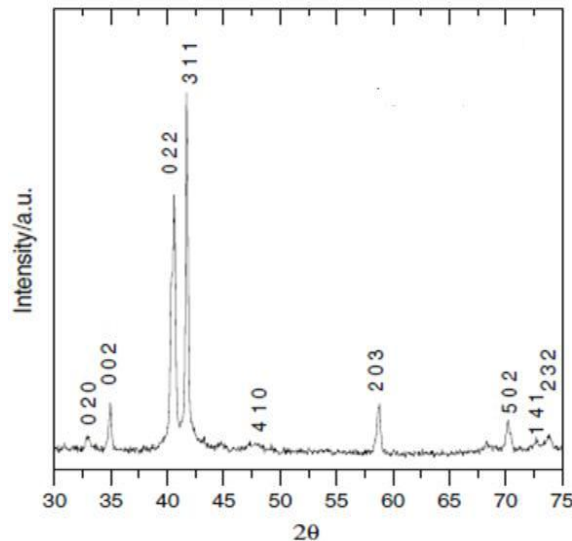


Fig 5. X-ray diffraction pattern of $Mn_{50}Ni_{42.5}Sn_{7.5}$ alloy.

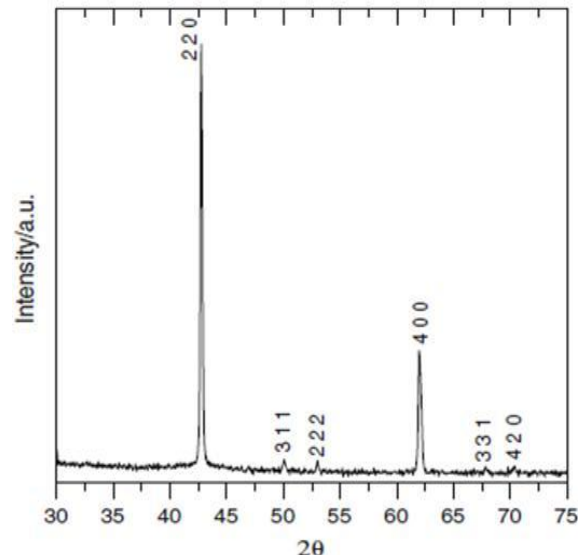


Fig 6. X-ray diffraction pattern at of $Mn_{50}Ni_{40}Sn_{10}$ alloy.

4. CONCLUSIONS

For $Ni_{50}Mn_{50-x}Sn_x$ ($x = 5, 7.5$ and 10) series Alloy, as the Sn content increases from 5 to 10, the transformation temperature from martensite to austenite decreases. From X-Ray analysis, the alloys with Sn5 and Sn7.5 has orthorhombic martensite phase whereas alloy with Sn10 has a martensite cubic L_21 phase.

5. REFERENCES

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