Prediction of Hydrostatic Head Effect in Process Plant Evaporators by Nomograph

____.G.K. Roy

E vaporation in process plant evaporators is influenced by two common phenomena, viz. **Solute** effect and **Hydrostatic head effect**, which elevate the boiling point of the solution thereby reducing the available temperature difference driving force for boiling heat transfer and increasing the heat transfer area. Although literature provides information in the form of plots and nomographs(^{1,2)} for a quick estimate of boiling point elevation for different solutes in their solutions, available information for the prediction of hydrostatic head effect is scanty^{'31}. The effect of hydrostatic head on the boiling heat transfer is quite appreciable in many situations and cannot be ignored especially for evaporators operating under moderate to high vacuum and when the liquid-level' is fairly high above the tube bundle.

In this communication a nomograph has been prepared for the rapid estimation of the hydrostatic head effect with the help of the following equation:

 $\Delta t_{\mathbf{h}} = 0.87 \nu_{\mathbf{R}} T_{\mathbf{R}} \Delta P \qquad (1)$

Where, $\Delta t_h = hydrostatic elevation of the boiling point, °C$

 T_R = Solution boiling temperature, °K v_R = specific volume of water vapour at T_R , m^3

kg

 λ = latent heat of vaporisation corresponding to the saturation pressure, Kcal-

kg

 ΔP = hydrostatic head, metre (one-half of the indicated liquid level)

Equation (1) is a converted form of equation (14-7) given by Kern⁽³⁾.

Figure-1 presents the nomograph for the direct prediction of the hydrostatic elevation of boiling point based on equation 1, Accuracy (valuation) of the nomograph:

The values obtained from nomograph coincide well with their respective values obtained from the equation 1.

EXAMPLE:

point.

Solution boiling temperature: (TR). 331.6° K specific volume of water vapour at T_R (ν _R): 8.164 m²

latent heat of vaporisation corresponding to saturation Kcal

pressure (λ): 564.03 — kg

hydrostatic head (ΔP): 1 meter To calculate and compare the hydrostatic elevation of boiling



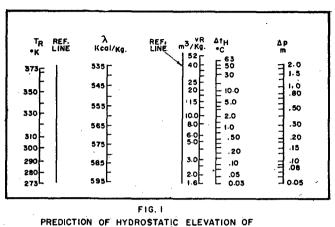
THE AUTHOR

Dr. G. K. Roy, Professor in Chemical Engineering. Dept. of Regional Engineering College, Rourkela, received B.Sc. Chem Engg. in 1966 from Banaras Hindu University, M. Tech in 1971, from IIT, Kharagpur; and Ph.D. in 1975, from the Sambalpur University. He was a post doctoral Fellow at the University of Karlsruhe, West Germany during 1977-78.

Author of more than 50 research publications and 5 books. Dr. Roy was awarded the Sir Gangaram Memorial Award in 1974 and Certificates of merit in 1978 and 1984 from the Institution of Engineers (India) for papers published in the Institution journal.

CEW

1



BOILING POINT.

SOLUTION

$$\Delta \text{ th} = 0.87 \nu_{\text{R}} \Gamma_{\text{R}} \Delta P$$
$$= 0.87 \times 8.164 \times 331.6 \times 331.$$

_____ = 4.18 ℃

from nomograph,
$$\Delta$$
 th = 4.0°C

561 02

Percentage deviation of nomograph value from the calculated ones = 4.3.

REFERENCES

- 1) Hougen O.A., Watson K.M. and Ragatez R.A. Chemical Process Principles, Vol. I, 2nd edition, John Wiley & Sons Inc., P 81 & 104 (Fig. 17)
- 2) Perry J.H., Chemical Engineers' Hand book, Fourth edition, P 11 & 30 (Fig.11 & 19)
- 3) Kern D.Q., Process Heat Transfer, McGraw Hill Book Co. Inc., P408.

